

## Chapter 14 – Fracture Mechanics

### Stress Concentrations

- discontinuities typically exist in structures (holes, cross-section changes, keyways, etc.)
- discontinuities  $\Rightarrow$  locally increase stress (stress raisers)
- $K_t$ , theoretical stress concentration factor, used to quantify stress magnification in critical location:

$$K_t = \sigma_m / \sigma_0$$

$\sigma_m$  - maximum stress

$\sigma_0$  - nominal stress

- note  $K_t$  is dimensionless
- designers use  $K_t$  data extensively for structural design
- shortcomings ?? based on elastic behavior; doesn't account for cracks; more significant for brittle materials

### Fracture Mechanics vs. Fracture Mechanisms

#### Fracture Mechanics:

- a specific mechanics approach to quantify failure
- assumes materials contain flaws and uses engineering mechanics methods to characterize crack growth behavior and crack instability

#### Fracture Mechanisms:

- defines failure processes in materials (microscopic and macroscopic)
- physical methods of failures (ex: intergranular separation, crazing, cleavage, etc.)

### Theoretical Cohesive Strength

#### Theoretical Predictions of Strength:

Separation of atomic planes in tension:

$$\sigma_c = [ E \gamma / a_0 ]^{1/2}$$

where:

- $\sigma_c$  is critical tensile stress for separation
- E is Young's Modulus
- $\gamma$  is surface energy of newly formed crack surface
- $a_0$  is equilibrium atomic spacing

and using simplifying assumptions:

$$\sigma_c \sim E / \pi$$

Shear of adjacent atomic planes:

$$\tau_c = G b / 2 \pi a$$

where:

- $\tau_c$  is critical shear stress to cause slip
- G is shear modulus
- B is the slip distance
- a is interplanar atomic spacing

and using simplifying assumptions:

$$\tau_c \sim G / 2 \pi$$

Substituting values of E and G into above equations and comparing to experimentally measured strengths, it is found these models predict theoretical strengths >>>> than observed strengths.

Why????  $\Rightarrow \Rightarrow \Rightarrow \Rightarrow$  defects in materials:

- flaws
- dislocations

\* Existence of dislocations postulated ~ 1930's

\* Concept of preexisting flaws: Griffith (1920)

## Griffith Approach

- \* Concept of preexisting flaws
- \* A crack propagates when the amount of elastic strain energy released exceeds the surface energy of the newly formed crack.

Thus for the following geometry stressed in tension:

infinitely wide, thin sheet

center crack of length  $2a$ , oriented normal to the stress direction

crack is elliptical, through-the-thickness

$$\sigma_c = [ 2 \gamma E / \pi a ]^{1/2}$$

where:

- $\sigma_c$  is critical tensile stress for crack instability
- $\gamma$  is surface energy of newly formed crack surface
- $E$  is Young's Modulus
- $a$  is half crack length

\* His early experimental results on glass verified this theory, but they were fortuitous

\* Initially proposed in 1920, but no significant acceptance until the late 1940's after Irwin and Orowan modifications

## Irwin Modification

In 1948 Orowan and Irwin showed the importance of local plastic deformation at the crack tip

Dissipative processes involved in fracture >>>>  $\gamma$  term envisioned by Griffith

Resulted in modified Griffith equation:

$$\sigma_c = [ G_c E / \pi a ]^{1/2}$$

where:

- $\sigma_c$  is critical tensile stress for crack instability
- $G_c$  is critical strain energy release rate (which equals  $\gamma + P$ , with  $P$  being a "plastic" dissipation of energy)
- $E$  is Young's Modulus
- $a$  is half crack length

Irwin showed equivalence to his newly developed stress intensity approach, which was the founding of Linear Elastic Fracture Mechanics (LEFM)

## Stress Intensity Approach

$$G = K^2 / E$$

where:

- G is strain energy release rate
- K is stress intensity factor
- E is Young's Modulus

thus for an infinitely wide, thin sheet containing a center, through-the-thickness crack of length 2a under a tensile stress  $\sigma$ :

$$K = \sigma [\pi a]^{1/2}$$

in general, for any cracked body:

$$K = Y \sigma [\pi a]^{1/2}$$

where Y is a geometric factor

at crack instability:

$$K_{Ic} = Y \sigma_c [\pi a_c]^{1/2}$$

where:

- "c" represents the critical condition
- $K_{Ic}$  is the critical stress intensity (for Mode I loading) and is called "plane strain fracture toughness", assuming certain validity aspects are maintained

## Nomenclature

### Types of Failure

- brittle vs. ductile
- brittle: little overall plastic deformation occurring before or during fracture
- ductile: appreciable plastic deformation occurring before or during fracture

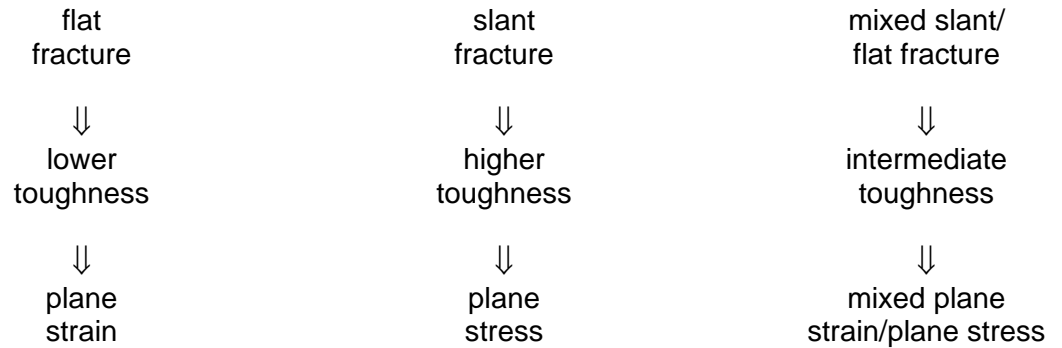
### "Toughness" or Toughness Measures

- area under stress – strain curve
- notched impact (e.g., Charpy)
- fracture toughness ( $K_{Ic}$ ,  $G_{Ic}$ )
- plasticity extent at stress concentration ( $r_y$ )

- notched-to-smooth tensile strength ratio
- others.....

## Macroscopic Failure Modes

### Surface Flatness



### Surface Markings

- fatigue beachmarks
- chevron markings
- stress corrosion areas
- fast fracture areas
- etc.

## Microscopic Failure Modes

### Surface Markings

metals – transgranular, intergranular, microvoid coalescence (dimpled rupture), cleavage, quasi-cleavage, .....

polymers – crazes, fibrils, hackles, mirror, .....

ceramics – mirror, mist, hackle, .....

### Plane Stress vs. Plane Strain

loads applied in plane of body

plane stress (thin sections):

$$\sigma_z = 0 \qquad \varepsilon_z \neq 0$$

plane strain (thick sections):

$$\sigma_z \neq 0 \qquad \varepsilon_z = 0$$

## Fracture Mechanics Terminology

Crack surface displacement modes:

Mode I - opening mode

Mode II - edge-sliding mode

Mode III - tearing mode

where: I, II, III are subscripted on G, K fracture mechanics terms, as applicable

Common fracture mechanics terms:

K - stress intensity factor

$K_I$  - mode I stress intensity factor

$K_{II}$  - mode II stress intensity factor

$K_{III}$  - mode III stress intensity factor

$K_{Ic}$  - mode I critical stress intensity factor; plane strain fracture toughness; fracture toughness

$K_c$  - often used to designate mode I plane stress fracture toughness (not universally accepted)

$\Delta K$  - range in stress intensity factor in fatigue loading cycle

G - strain energy release rate or crack extension force

$G_{Ic}$  - mode I critical strain energy release rate or crack extension force; fracture toughness

## Application Areas of Fracture Mechanics

### Critical Crack Instability

- quasi-static fracture toughness:  $K_{Ic}$
- dynamic fracture toughness:  $K_{IId}$

## Subcritical Crack Growth

- fatigue crack propagation:  $da/dN$  vs.  $\Delta K$
- environmentally assisted crack growth:  
 $K_I$  vs.  $da/dt$        $K_{Isc}$        $K_{IEAC}$        $t_f$

## Typical Fracture Mechanics Applications

- fracture instability
- fatigue crack propagation/retardation effects
- stress corrosion
- stress corrosion/fatigue
- hydrogen embrittlement
- proof testing of pressure vessel
- failure analysis

## Areas of Fracture Mechanics Utilization

- aircraft components
- turbines
- rockets and missiles
- oil industry
- nuclear industry
- rock mechanics
- rail transportation
- marine applications

## Historical Development

- 1958 Department of Defense, ASTM initiate study of fracture problems in rocket propellant tanks
- 1959 ASTM Committee E24 on Fracture Toughness Testing of Metallic Materials formed
- 1964 First symposium devoted solely to sharp crack fracture mechanics  
Paris (Lehigh Univ.) proposes use of stress intensity for correlating fatigue crack propagation

- 1965 Brown (NRL) first to employ precracked fracture mechanics specimens to stress corrosion studies
- NASA pressure vessel failures – requirement for fracture mechanics qualification of pressure vessel materials and proof test fluids
- 1969 Critical defect in F-111 steel wing pivot fitting
- 1972 ASTM adopts standard fracture toughness testing procedures (E399)
- U. S. Air Force develops Aircraft Structural Integrity Program (MIL-STD-1530)
- 1974 U. S. Air Force develops Airplane Damage Tolerant Design Requirements (MIL-A-83444)
- 1979 British develop methods for Crack-Tip-Opening-Displacement (CTOD) Testing (BS5762)
- 1981 ASTM adopts standard practice for R-Curve determination (E561)
- 1985 ASTM adopts standard for  $J_{IC}$  testing (E813)
- Many subsequent additions/modifications to many applications
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