

Solution 12.1 :-

Infinite plate of unit thickness.

$$2a_0 = 0.5''$$

$$K_{Ic} = 80 \text{ KSI} \sqrt{\text{in}}$$

$$E = 10 \times 10^6 \text{ psi. } \nu = 0.3$$

$$\sigma_{\max} = 60 \text{ ksi}$$

$$R = 0.1$$

$$R = \frac{\sigma_{\min}}{\sigma_{\max}}$$

$$\therefore \sigma_{\min} = 6$$

$$\frac{da}{dN} = 1.6 \times 10^{-12} (\Delta K)^4$$

$$a) \quad K_{Ic} = \sigma_{\max} \sqrt{\pi a_f}$$

$$80 = 60 \sqrt{\pi a_f}$$

$$\therefore a_f = 0.5658 \text{ in}$$

From fatigue crack growth

$$N_f = \frac{1}{C \pi^2 (\Delta \sigma)^4} \left[ \frac{1}{a_0} - \frac{1}{a_f} \right]$$

$$= \frac{1}{1.6 \times 10^{-12} \times \pi^2 \times (60-6)^4} \left[ \frac{1}{0.25} - \frac{1}{0.5658} \right]$$

$$= 16627 \text{ cycles. } N_f = 16,630 \text{ cycles}$$

b) Maximum crack opening displacement at time of failure  
Considering loading as mode I

$$u_y = \frac{K_I}{8\mu} \sqrt{\frac{2r}{\pi}} \left[ (2k-1) \sin \frac{\theta}{2} - \sin \frac{3\theta}{2} \right]$$

Considering plane strain

$$\mu = \frac{E}{2(1+\nu)} = \frac{10 \times 10^6}{2(1+0.3)} = 3.846 \times 10^6$$

$$k = 3 - 4\nu = 3 - 4(0.3) = 1.8$$

$$u_y = \frac{80,000}{8 \times 3.846 \times 10^6} \sqrt{\frac{2 \times 0.5658}{\pi}} \left[ (2 \times 1.8 - 1) \sin 90^\circ - \sin 270^\circ \right]$$

$$= 0.00874 \text{ in}$$

$$\begin{aligned} \therefore \text{Maximum crack opening displacement} \\ = 2u_y = 0.0174 \text{ in} \end{aligned}$$

c) Residual strength of plate after  $4 \times 10^3$  fatigue life

$$N_f = \frac{1}{C \times \pi^2 \times (\Delta \sigma)^4} \left[ \frac{1}{a_0} - \frac{1}{a_1} \right]$$

$$4 \times 10^3 = \frac{1}{1.6 \times 10^{-12} \times \pi^2 \times (54)^4} \left[ \frac{1}{0.25} - \frac{1}{a_1} \right]$$

$$a_1 = 0.2887 \text{ in} \approx 0.289 \text{ in}$$

$$\begin{aligned} \therefore \text{Residual strength } \sigma_c &= \frac{K_{Ic}}{\sqrt{\pi \cdot a_c}} \\ &= \frac{80000}{\sqrt{\pi \cdot 0.2887}} = 83991 \text{ psi} \\ &= 84.0 \text{ ksi} \end{aligned}$$

d) By crack size  $2a_0 = 1 \text{ in}$

$$\begin{aligned} \text{i) } N_f &= \frac{1}{(1.6 \times 10^{-12}) \pi^2 \times (54)^4} \left[ \frac{1}{0.5} - \frac{1}{0.5658} \right] \\ &= 1732 \text{ cycles} \end{aligned}$$

ii) Maximum crack opening displacement remain unchanged

iii)  $N_f = 4 \times 10^3$  cycles is greater than  $N_f = 1732$  cycles so it will not be able to this loading cycle.

Solution 12.2 :

$$S_{ult} = 150 \text{ ksi}$$

$$S_e = 50 \text{ ksi}$$

$$S_{1000} = 100 \text{ ksi}$$

$$\sigma_f = 175 \text{ ksi}$$

a) For Load 1

$$\sigma_{max} = 60 \text{ ksi} \quad \sigma_{min} = 0 \quad n_1 = 50,000 \text{ cycles}$$

$$\sigma_a = \frac{\sigma_{max} - \sigma_{min}}{2} = 30 \text{ ksi}$$

$$\sigma_m = \frac{\sigma_{max} + \sigma_{min}}{2} = 30 \text{ ksi}$$

By using Goodman relationship

$$\frac{\sigma_a}{S_n} + \frac{\sigma_m}{S_{ult}} = 1$$

$$\frac{30}{S_n} + \frac{30}{150} = 1 \quad S_n = 37.5 \text{ ksi}$$

Also,  $S_n = a(N_1)^b$

$$a = \frac{S_{1000}^2}{S_e} = \frac{(100)^2}{50} = 200$$

$$b = -\frac{1}{3} \log\left(\frac{S_{1000}}{S_e}\right) = -\frac{1}{3} \log\left(\frac{100}{50}\right) = -0.1003$$

$$S_n = 37.5 \text{ ksi} = 200(N_1)^{-0.1003}$$

$$\Rightarrow \text{cycles to fail by 1} \rightarrow N_1 = 17710 \times 10^3 \text{ cycles}$$

For Load 2

$$\sigma_{max} = 90 \text{ ksi} \quad \sigma_{min} = 30 \text{ ksi} \quad n_2 = 30,000 \text{ cycles}$$

$$\sigma_a = 30 \text{ ksi} \quad \sigma_m = 60 \text{ ksi}$$

By Goodman relationship

$$\frac{30}{S_n} + \frac{60}{150} = 1$$

$$S_n = 50 \text{ ksi}$$

$$S_n = a N_2^b$$

$$50 = 200 (N_2)^{-0.1003}$$

$$N_2 = 1006 \times 10^3 \text{ cycles}$$

cycle to fail for segment 2.

b) Fatigue Damage at the end of 1<sup>st</sup> block of loading

$$\begin{aligned} D_1 &= \frac{n_1}{N_1} + \frac{n_2}{N_2} \\ &= \frac{50 \times 10^3}{17710 \times 10^3} + \frac{30 \times 10^3}{1006 \times 10^3} \\ &= 0.0326 \end{aligned}$$

c) Fatigue life if block loading is repeated

$$\text{Total fatigue life } N_f = \frac{1}{0.0326} = 30.675 \text{ blocks.}$$

That means 30 full blocks, and fraction of either block I or II, to find that

$$\begin{aligned} \text{damage due to } 0.675 \text{ block} &= 0.675 \times 0.0326 \\ &= 0.022 \end{aligned}$$

$$\begin{aligned} \text{Now, damage due to load 1} &= \frac{n_1}{N_1} = \frac{2.823 \times 10^3}{\approx 0.00282} \\ \text{load 2} &= \frac{n_2}{N_2} = 0.0298 \end{aligned} \left. \vphantom{\begin{aligned} \text{Now, damage due to load 1} \\ \text{load 2} \end{aligned}} \right\} \text{ in a block}$$

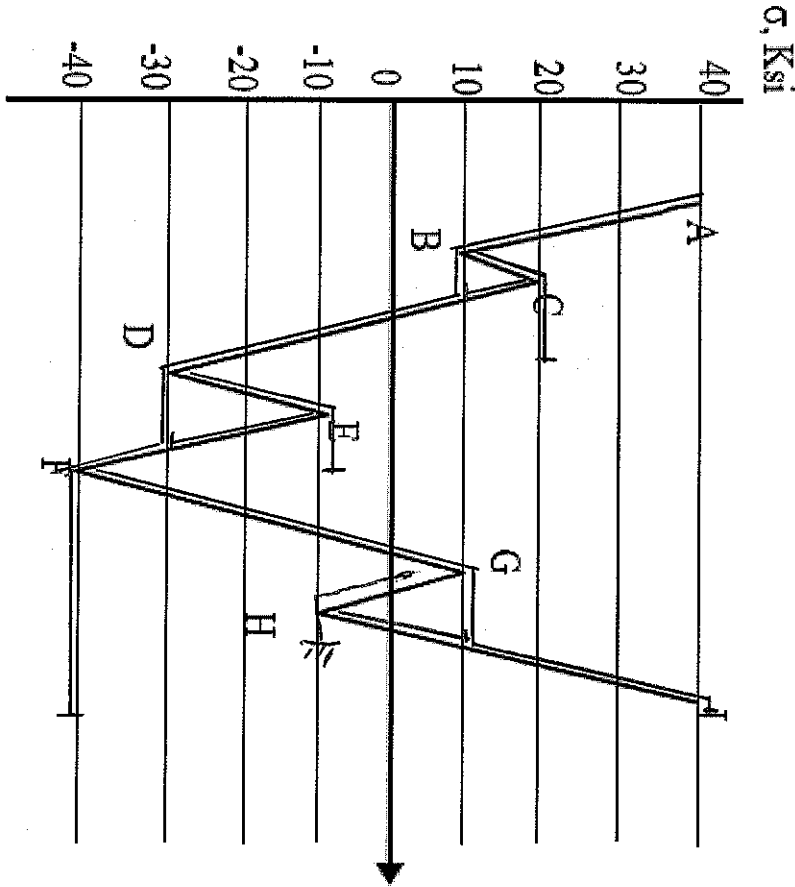
Damage in 31<sup>st</sup> block

$$\begin{array}{rcc} \text{Total} & \text{load 1} & \text{load 2} \\ 0.022 & = & 0.00282 + \frac{\text{No. of cycles}}{1006 \times 10^3} \end{array}$$

$$\text{No. of cycles} = 19291$$

$$\begin{aligned} \text{Fatigue life} &= 30 \text{ blocks} + (50,000)_{\text{cycles load 1}} + (19291)_{\text{cycles load 2}} \\ &= 30(50,000 + 30,000) + 50,000 + 19291 \\ &= 2469291 \text{ cycles} \end{aligned}$$

Solution 12.3:- a) Rainflow Method



Cycle	Range
ABDF - FGI	80
BC - CB	10
DE - ED	20
GH - HG	20

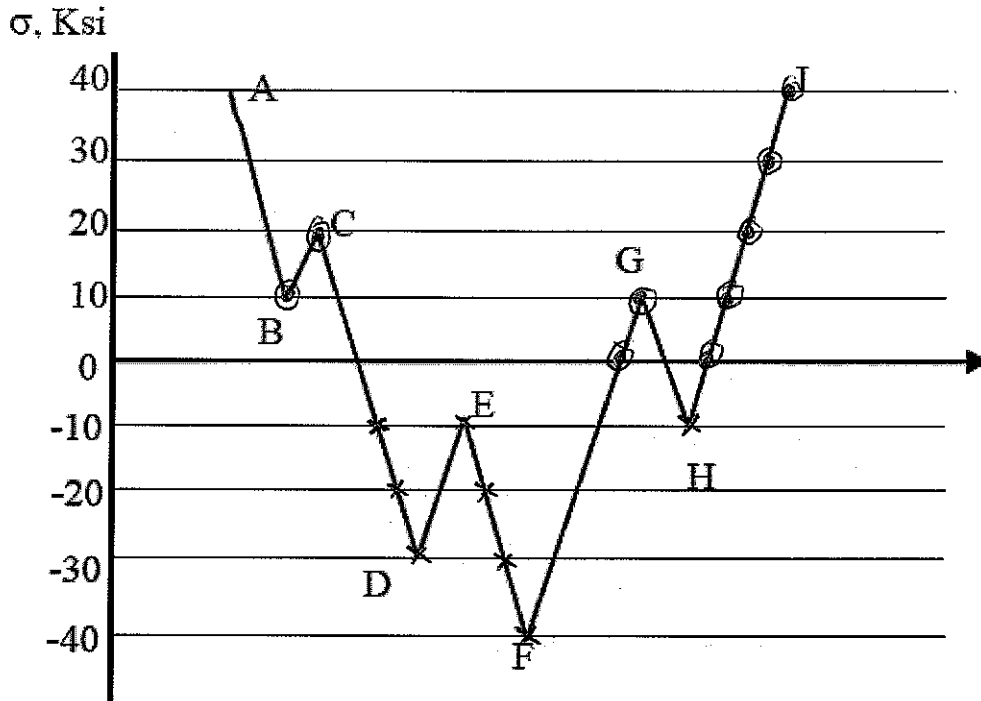
b) Peak Counting Method

Level	Range
AF	80
CD	50
GE	20

c) Simple Range Counting

Strain Level	Cycle Counts	Range (Levels)	Cycle Counts
AB	0.5		
BC	0.5		
CD	0.5	50	1.5
DE	0.5	30	1.0
EF	0.5	20	1.0
FG	0.5	10	0.5
GH	0.5		
HI	0.5		

d) Level Crossing Method



Level	Counts	Revised Count	Revised Count
40	1	0	-
30	1	0	-
20	2	1	0
10	3	2	1
0	2	1	0
-10	3	2	1
-20	2	1	0
-30	2	1	0
-40	1	0	-

Pairing level	Counts	Range Level
40 & -40	1	80
20 & -30	1	50
10 & -10	1	20