

**MAE3315**  
**Homework No.2 (SOLUTION)**

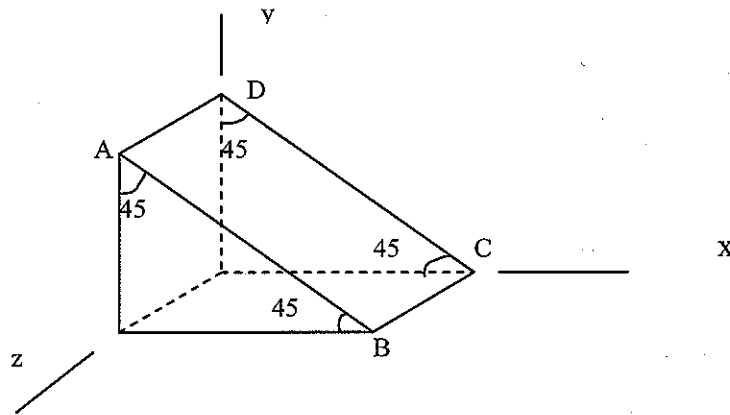
**Problem 2-1**

A state of stress is given at a point on the vertical fin of an aircraft as

$$[\sigma] = \begin{bmatrix} \sigma_x & \tau_{xy} \\ \tau_{xy} & \sigma_y \end{bmatrix} = \begin{bmatrix} 30 & 4 \\ 4 & 10 \end{bmatrix} \text{ Ksi}$$

Find

- a) The normal and shear stress components on the plane ABCD.
- b) The corresponding stress components if the original plane is rotated  $45^\circ$  about the z-axis.



**Solution:**

a)

First, we need the projection of  $\{n\}$  on  $\{x\}$  and  $\{y\}$ .

$$n_x = \cos(\theta) = \cos(45) = \frac{1}{\sqrt{2}} \quad \text{and} \quad n_y = \sin(\theta) = \sin(45) = \frac{1}{\sqrt{2}}$$

Therefore, the vector  $\{n\}$  becomes,

$$\{n\} = \begin{Bmatrix} 1/\sqrt{2} \\ 1/\sqrt{2} \end{Bmatrix}$$

On the other hand,  $\{t\} = [\sigma] \cdot \{n\}$ ,

$$\begin{Bmatrix} t_x \\ t_y \end{Bmatrix} = \begin{bmatrix} 30 & 4 \\ 4 & 10 \end{bmatrix} \cdot \begin{Bmatrix} 1/\sqrt{2} \\ 1/\sqrt{2} \end{Bmatrix} = \begin{Bmatrix} 34/\sqrt{2} \\ 14/\sqrt{2} \end{Bmatrix}$$

Finally,  $\sigma_n = \vec{t} \cdot \vec{n}$ ,

$$\sigma_n = \vec{t} \cdot \vec{n} = t_x n_x + t_y n_y = \left(\frac{34}{\sqrt{2}}\right)\left(\frac{1}{\sqrt{2}}\right) + \left(\frac{14}{\sqrt{2}}\right)\left(\frac{1}{\sqrt{2}}\right) = \frac{34}{2} + \frac{14}{2} = 24 \text{Ksi}$$

Now,

$$\sigma_n^2 + S^2 = \|\vec{t}\|^2$$

$$S = \sqrt{\|\vec{t}\|^2 - \sigma_n^2}$$

Where,

$$\|\vec{t}\| = \sqrt{t_x^2 + t_y^2} = \sqrt{\left(\frac{34}{\sqrt{2}}\right)^2 + \left(\frac{14}{\sqrt{2}}\right)^2} = \sqrt{578 + 98} = 26 \text{Ksi}$$

$$S = \sqrt{(26)^2 - (24)^2}$$

$$S = 10 \text{Ksi}$$

With,

$$\vec{\tau} = \frac{\vec{t} - \sigma_n \vec{n}}{S}$$

$$\vec{\tau} = \frac{\begin{Bmatrix} 34/\sqrt{2} \\ 14/\sqrt{2} \end{Bmatrix} - 24 \begin{Bmatrix} 1/\sqrt{2} \\ 1/\sqrt{2} \end{Bmatrix}}{10} = \begin{Bmatrix} 1/\sqrt{2} \\ -1/\sqrt{2} \end{Bmatrix}$$

This means that the direction of the Shear Stress is negative in our convention. Therefore,  $S = -10 \text{ksi}$ . **There is another way to solve for the Shear Stress,**

To calculate the components of the vector  $\{\tau\}$ ,

$$\tau_x = -\sin(\theta) = -\sin(45) = -\frac{1}{\sqrt{2}} \quad \text{and} \quad \tau_y = \cos(\theta) = \cos(45) = \frac{1}{\sqrt{2}}$$

As a result, the vector  $\{\tau\}$  becomes,

$$\{\tau\} = \begin{Bmatrix} -1/\sqrt{2} \\ 1/\sqrt{2} \end{Bmatrix}$$

And then,  $S = \vec{t} \cdot \vec{\tau}$ ,

$$S = \vec{t} \cdot \vec{\tau} = t_x \tau_x + t_y \tau_y = \left(\frac{34}{\sqrt{2}}\right)\left(\frac{-1}{\sqrt{2}}\right) + \left(\frac{14}{\sqrt{2}}\right)\left(\frac{1}{\sqrt{2}}\right) = \frac{-34}{2} + \frac{14}{2} = -10 \text{Ksi}$$

b)

$$[\sigma_{x'-y'}] = [T_\sigma(\theta)][\sigma_{x-y}]$$

$$\begin{bmatrix} \sigma_{x'} \\ \sigma_{y'} \\ \tau_{x'y'} \end{bmatrix} = \begin{bmatrix} m^2 & n^2 & 2mn \\ n^2 & m^2 & -2mn \\ -mn & mn & m^2 - n^2 \end{bmatrix} \cdot \begin{bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{bmatrix} \quad \text{where, } \begin{cases} m = \cos \theta \\ n = \sin \theta \end{cases}$$

$$\begin{bmatrix} \sigma_{x'} \\ \sigma_{y'} \\ \tau_{x'y'} \end{bmatrix} = \begin{bmatrix} (1/\sqrt{2})^2 & (1/\sqrt{2})^2 & 2(1/\sqrt{2})(1/\sqrt{2}) \\ (1/\sqrt{2})^2 & (1/\sqrt{2})^2 & -2(1/\sqrt{2})(1/\sqrt{2}) \\ -(1/\sqrt{2})(1/\sqrt{2}) & (1/\sqrt{2})(1/\sqrt{2}) & (1/\sqrt{2})^2 - (1/\sqrt{2})^2 \end{bmatrix} \cdot \begin{bmatrix} 30 \\ 10 \\ 4 \end{bmatrix} \text{Ksi}$$

$$\begin{bmatrix} \sigma_{x'} \\ \sigma_{y'} \\ \tau_{x'y'} \end{bmatrix} = \begin{bmatrix} 1/2 & 1/2 & 1 \\ 1/2 & 1/2 & -1 \\ -1/2 & 1/2 & 0 \end{bmatrix} \cdot \begin{bmatrix} 30 \\ 10 \\ 4 \end{bmatrix} \text{Ksi}$$

$$\begin{bmatrix} \sigma_{x'} \\ \sigma_{y'} \\ \tau_{x'y'} \end{bmatrix} = \begin{bmatrix} 24 \\ 16 \\ -10 \end{bmatrix} \text{Ksi}$$

Same results as part a, as expected!

**Problem 2-2**

A stress state at a point **P** on a plane is given as below.

$$[\sigma] = \begin{bmatrix} 1 & -3 & 5 \\ -3 & 2 & 2 \\ 5 & 2 & 3 \end{bmatrix} \cdot 10^3 \text{ Psi}$$

Consider a plane,  $4x + 3y + 6z = 12$  through the point **P**.

- Find the normal component of the traction  $\sigma_n$  and its tangential component **S** acting at that point **P** on this plane.
- Find the direction cosines of  $\sigma_n$  and **S**.
- Find the magnitude of the traction vector **t** and its angle with the normal vector **n**

**Solution:**

a)

First, we need to find the directional cosines of that plane  $4x + 3y + 6z = 12$ . From this equation is easy to compute that:  $a=3$ ,  $b=4$ , and  $c=2$ .

$$\text{Cos}\alpha = \frac{bc}{\sqrt{(bc)^2 + (ac)^2 + (ab)^2}} = \frac{(4)(2)}{\sqrt{((4)(2))^2 + ((3)(2))^2 + ((3)(4))^2}} = 0.5121 = l$$

$$\text{Cos}\beta = \frac{ac}{\sqrt{(bc)^2 + (ac)^2 + (ab)^2}} = \frac{(3)(2)}{\sqrt{((4)(2))^2 + ((3)(2))^2 + ((3)(4))^2}} = 0.3841 = m$$

$$\text{Cos}\gamma = \frac{ab}{\sqrt{(bc)^2 + (ac)^2 + (ab)^2}} = \frac{(3)(4)}{\sqrt{((4)(2))^2 + ((3)(2))^2 + ((3)(4))^2}} = 0.7682 = n$$

$$\vec{n} = \begin{Bmatrix} 0.5121 \\ 0.3841 \\ 0.7682 \end{Bmatrix}$$

As we know,  $\{t\} = [\sigma] \cdot \{n\}$ ,

$$\{t\} = \begin{bmatrix} 1 & -3 & 5 \\ -3 & 2 & 2 \\ 5 & 2 & 3 \end{bmatrix} \text{Ksi} \begin{Bmatrix} 0.5121 \\ 0.3841 \\ 0.7682 \end{Bmatrix} = \begin{Bmatrix} 3.2009 \\ 0.7682 \\ 5.6336 \end{Bmatrix} \text{Ksi}$$

$$\|\vec{t}\| = \sqrt{(3.2009)^2 + (0.7682)^2 + (5.6336)^2} = 6.5249 \text{ Ksi}$$

Finally,  $\sigma_n = \vec{t} \cdot \vec{n}$ ,

$$\sigma_n = \vec{t} \cdot \vec{n} = t_x n_x + t_y n_y + t_z n_z = (3.2009)(0.5121) + (0.7682)(0.3841) + (5.6336)(0.7682) = 6.2623 \text{ Ksi}$$

And,

$$\sigma_n^2 + S^2 = \|\vec{t}\|^2$$

$$S = \sqrt{\|\vec{t}\|^2 - \sigma_n^2}$$

$$S = \sqrt{(6.5249)^2 - (6.2623)^2} = 1.8323 \text{ Ksi}$$

b)

The directional cosines of  $\sigma_n$  is naturally  $\{n\}$ ,

$$\vec{n} = \begin{Bmatrix} 0.5121 \\ 0.3841 \\ 0.7682 \end{Bmatrix}$$

And the directional cosines of  $\vec{\tau}$  are,

$$\vec{\tau} = \frac{\vec{t} - \sigma_n \vec{n}}{S}$$

$$\vec{\tau} = \frac{\begin{Bmatrix} 3.2009 \\ 0.7682 \\ 5.6336 \end{Bmatrix} - 6.2623 \begin{Bmatrix} 0.5121 \\ 0.3841 \\ 0.7682 \end{Bmatrix}}{1.8323} = \begin{Bmatrix} -0.0034 \\ -0.8935 \\ 0.4490 \end{Bmatrix}$$

c)

The magnitude of  $\{\vec{t}\}$  was already calculated,

$$\|\vec{t}\| = 6.5249 \text{ Ksi}$$

To calculate the angle, we know that,

$$\tan \theta = \frac{S}{\sigma_n}$$

$$\theta = \text{ArcTan}\left(\frac{S}{\sigma_n}\right) = 0.2847 \text{ radians} = 16.3^\circ$$

**Another way to solve it,**

$$[\vec{t}] \cdot [\hat{n}] = \|\vec{t}\| \|\hat{n}\| \cos \theta$$

$$\theta = \text{ArcCos}\left(\frac{[\vec{t}] \cdot [\hat{n}]}{\|\vec{t}\|}\right)$$

$$\theta = \text{ArcCos}\left(\frac{\sigma_n}{\|\vec{t}\|}\right)$$

$$\theta = \text{ArcCos}\left(\frac{6.2623 \text{ MPa}}{6.5249 \text{ MPa}}\right)$$

$$\theta = 16.3^\circ$$

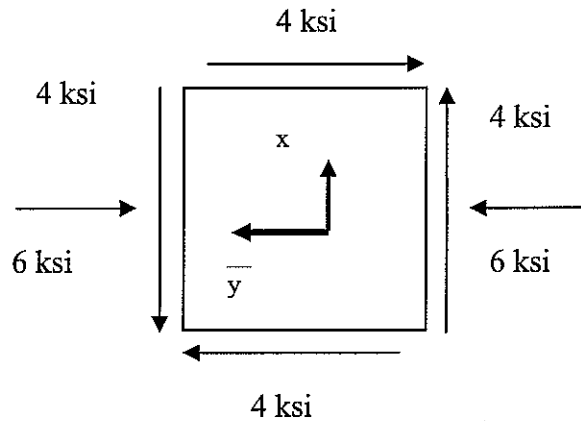
Same answer as expected!

**Problem 2-3**

A stress element has the state of stress as shown below:

Find the principal stresses and their corresponding directions.

Note: Use the method given in the class only.



**Solution:**

$$[\sigma] = \begin{bmatrix} 0 & -4 \\ -4 & -6 \end{bmatrix} \text{ksi}$$

$$\begin{vmatrix} 0 - \sigma_p & -4 \\ -4 & -6 - \sigma_p \end{vmatrix} = (-\sigma_p)(-6 - \sigma_p) - 16 = 0$$

$$(-\sigma_p)(-6 - \sigma_p) - 16 = 0$$

$$\sigma_p^2 + 6\sigma_p - 16 = 0$$

Therefore, the principal stresses are:

$$\begin{cases} \sigma_1 = 2 \text{Ksi} \\ \sigma_2 = 0 \text{Ksi} \\ \sigma_3 = -8 \text{Ksi} \end{cases}$$

For  $\sigma_1 = 2 \text{Ksi}$ :

$$\begin{bmatrix} 0 - 2 & -4 \\ -4 & -6 - 2 \end{bmatrix} \cdot \begin{Bmatrix} n_x^{(1)} \\ n_y^{(1)} \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}$$

$$\begin{cases} -2n_x^{(1)} - 4n_y^{(1)} = 0 \\ (n_x^{(1)})^2 + (n_y^{(1)})^2 = 1 \end{cases}$$

$$\begin{cases} n_x^{(1)} \\ n_y^{(1)} \end{cases} = \begin{cases} 2/\sqrt{5} \\ -1/\sqrt{5} \end{cases}$$

For  $\sigma_3 = -8Ksi$ :

$$\begin{bmatrix} 0 - (-8) & -4 \\ -4 & -6 - (-8) \end{bmatrix} \cdot \begin{cases} n_x^{(3)} \\ n_y^{(3)} \end{cases} = \begin{cases} 0 \\ 0 \end{cases}$$

$$\begin{cases} 8n_x^{(3)} - 4n_y^{(3)} = 0 \\ (n_x^{(3)})^2 + (n_y^{(3)})^2 = 1 \end{cases}$$

$$\begin{cases} n_x^{(3)} \\ n_y^{(3)} \end{cases} = \begin{cases} 1/\sqrt{5} \\ 2/\sqrt{5} \end{cases}$$